

Lecture 35

No Lecture
Friday

Nov. 16
2011
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Previously Flux across curve C ,

Divergence theorem $\int_C \mathbf{F} \cdot \mathbf{n} ds = \iint_D \text{div } \mathbf{F} dA$.

Flux across surface S $\iint_S \mathbf{F} \cdot \mathbf{n} dS$.

Today Divergence theorem for surfaces.

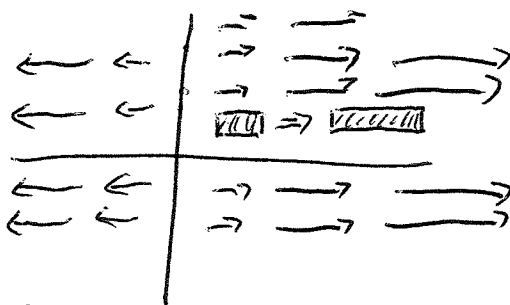
$\mathbf{F}: \mathbb{R}^3 \rightarrow \mathbb{R}^3$, divergence is

$$\text{div } (\vec{F}) = \frac{\partial F_1}{\partial x} + \frac{\partial F_2}{\partial y} + \frac{\partial F_3}{\partial z} = \nabla \cdot \vec{F}$$

~~Divergence theorem~~

Divergence measures compression/expansion of fluid/gas.

Ex $\vec{F}(x, y) = (x, 0)$
 $= x \hat{i}$



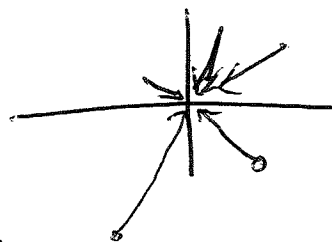
Gas expanding

$$\text{div } \vec{F} = \frac{\partial}{\partial x}(x) + \frac{\partial}{\partial y}(0) = 1 > 0.$$

Ex $\vec{F}(x, y) = (-x, -y)$

Liquid being compressed

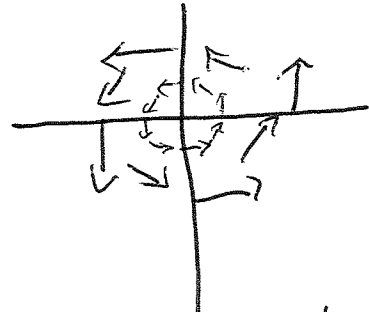
towards $(0, 0)$. Expect $\text{div } \vec{F} < 0$.



$$\text{div } \vec{F} = \frac{\partial}{\partial x}(-x) + \frac{\partial}{\partial y}(-y) = -1 + -1 = -2 < 0.$$

Flow lines: curve C param by $\vec{r}(t)$, so that $\vec{r}'(t) = \vec{F}(\vec{r}(t))$.

Ex $\vec{F}(x, y) = (-y, +x)$

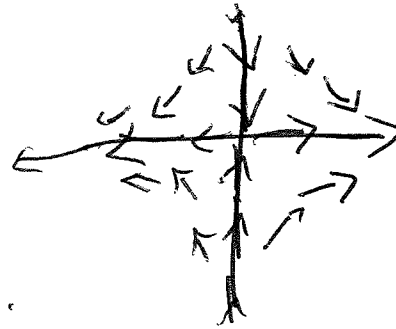


The "flow lines" are circles.

Region of gas rotated, not compressed. Expect $\text{div } \vec{F} = 0$.

$$\text{div } \vec{F} = \frac{\partial}{\partial x}(-y) + \frac{\partial}{\partial y}(x) = 0 + 0 = 0.$$

Ex $\vec{F}(x, y) = (x, -y)$



"Flow lines" are hyperbolas
(level curves of $g(x, y) = xy$).

Compression/Expansion less clear.

$$\text{div } \vec{F} = \frac{\partial}{\partial x} x + \frac{\partial}{\partial y}(-y) = 1 + (-1) = 0.$$

For one branch of hyperbola $xy = c$,
use parametrization $\vec{r}(t) = (e^t, c e^{-t})$.

Flow lines solutions to differential equations.

If $\text{div}(\vec{F})(x, y) > 0$, point (x, y) called a "source".

If $\text{div}(\vec{F})(x, y) < 0$, point (x, y) called a "sink".

How to think about divergence theorem for curves:

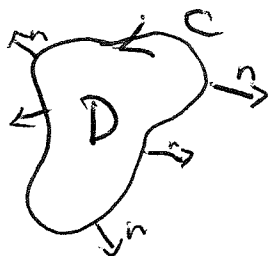
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$$\text{Flux} \nearrow \int_{\partial D} \vec{F} \cdot \vec{n} \, dS = \iiint_D \text{div } \vec{F} \, dV.$$

↑
amount of fluid
escaping D through
 C



infinite sum of
all sources (expansion $\rightarrow$ torque)
minus sum of all sinks
(compression $\rightarrow$ rotation)

The Divergence Theorem for surfaces (aka Gauss' Theorem)

Surface $S = \text{boundary of region } E \text{ in } \mathbb{R}^3$ must be "nice enough"
Assume components of $\vec{F}$ have continuous partials.

Then
$$\iint_S \vec{F} \cdot d\vec{S} = \iiint_E \text{div } \vec{F} \, dV.$$

Same intuition: amount of fluid pushed across
boundary determined by compression/expansion inside E .

(Using $\vec{n}$ pointing outwards to compute Flux).

Why? Write $\vec{F} = P\vec{e}_1 + Q\vec{e}_2 + R\vec{e}_3$.

Then LHS =
$$\iint_S (P\vec{e}_1 + Q\vec{e}_2 + R\vec{e}_3) \cdot \vec{n} \, dS$$

$$= \iint_S P(\vec{e}_1 \cdot \vec{n}) \, dS + \iint_S Q(\vec{e}_2 \cdot \vec{n}) \, dS + \iint_S R(\vec{e}_3 \cdot \vec{n}) \, dS$$

$$\text{RHS} = \iiint_E \left(\frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} + \frac{\partial R}{\partial z} \right) dV$$

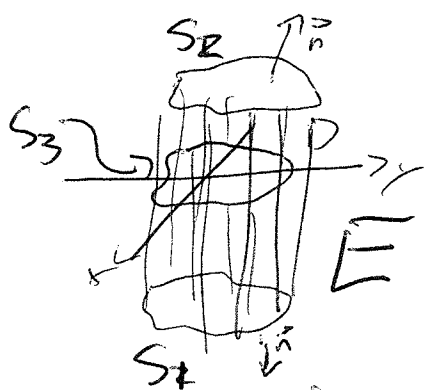
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So enough to identify 3 pieces from each equation. For example, want

$$\iint_S R(\vec{r} \cdot \vec{n}) dS = \iiint_E \frac{\partial R}{\partial z} dV.$$

Suppose E nice: "top" S_2 of E described by $z = f_2(x, y)$,
"bottom" S_1 " $z = f_1(x, y)$.

Then
$$\iiint_E \frac{\partial R}{\partial z} dV = \iint_D \int_{f_1}^{f_2} \frac{\partial R}{\partial z} dz dx dy.$$



$$= \iint_D R(x, y, f_2) - R(x, y, f_1) dx dy.$$

On the other hand,

$$\iint_S R(\vec{r} \cdot \vec{n}) dS = \iint_{S_1} R(\vec{r} \cdot \vec{n}) dS + \iint_{S_2} R(\vec{r} \cdot \vec{n}) dS$$

On S_3 $\vec{r} \cdot \vec{n} = 0 \implies \cancel{\iint_{S_3} R(\vec{r} \cdot \vec{n}) dS}.$

On S_1 , $\vec{n} = \frac{(-\frac{\partial f_1}{\partial x}, -\frac{\partial f_1}{\partial y}, -1)}{\| \cdot \|}$

so $\vec{r} \cdot \vec{n} = \frac{-1}{\sqrt{[\frac{\partial f_1}{\partial x}]^2 + [\frac{\partial f_1}{\partial y}]^2 + 1}} \leq \| \vec{r}_x \times \vec{r}_y \|$ ~~if~~

$$\iint_{S_1} R \cdot \frac{-1}{\| \vec{r}_x \times \vec{r}_y \|} dS = \iint_D R(x, y, f_1) \frac{-1}{\| \vec{r}_x \times \vec{r}_y \|} \| \vec{r}_x \times \vec{r}_y \| dA = - \iint_D R(x, y, f_1) dA.$$

Same idea shows $\iint_{S_2} R \cdot \vec{n} dS = \iiint_D R(x,y,z) dV$ (5) Nov-16

Ex $F = (zx, yz, z^2)$, S unit sphere.

Find flux.

$$\iint_S F \cdot dS = \iiint_{E=\text{Solid sphere}} \operatorname{div} F dV = \iiint_E z + zy + zx dV.$$

$$= z \iiint_E dV + z \iiint_E y dV + z \iiint_E x dV.$$

$$= z \operatorname{Vol}(E) = z \cdot \frac{4}{3}\pi = \frac{8}{3}\pi.$$

0 since region E symmetric across

In detail $\iiint_E y dV = \int_{-1}^1 \int_{-\sqrt{1-z^2}}^{\sqrt{1-z^2}} \int_{-\sqrt{1-x^2-z^2}}^{\sqrt{1-x^2-z^2}} y dy dx dz$

$y=0$ or $z=0$ planes.

0 since y is odd.

Topics for after Thanksgiving:

curl, conservative vector fields in $\mathbb{R}^3$, Stokes's Theorem

